

# Renewable and Alternative Energies

## Topic 2. Solar thermal energy project



**Pablo Castro Alonso**

Department of Electrical and Energy Engineering

This work is published under a license:

[Creative Commons BY-NC-SA 4.0](https://creativecommons.org/licenses/by-nc-sa/4.0/)

- **Description:**

- 5 floors. 40 homes (20 of 2 bedrooms and 20 of 3 bedrooms). Residential building in Valencia.



- **Objective:**

- Design of an FPC installation on the building roof for Domestic Hot Water (DHW). Energy production and demand. Storage system volume.
- Closed forced system.

- **Normative:**

- Código Técnico de Edificación. Documento “Ahorro energía” (CTE-HE4) (09/2013).
- Reglamento de instalaciones térmicas en los edificios (RITE) (09/2013).
- Instalación eléctrica (REBT).
- Normas UNE.

### Geographic and environmental data

City	Valencia
Latitude	39.48°
Altitude. m	10
Minimum winter T. °C	0
Historical minimum T. °C	-8
Climatic zone	IV

	Water T	Ambient average T	Absorber average T	Incident solar radiation kWh/(m <sup>2</sup> · day)
Month	°C	°C	°C	
1	10	10.0	15	2.96
2	11	11.0	15	3.80
3	12	13.0	20	4.76
4	13	15.0	20	5.08
5	15	18.0	25	5.21
6	17	22.0	30	5.57
7	19	24.0	30	6.08
8	20	24.0	30	5.92
9	18	22.0	30	5.57
10	16	18.0	25	4.63
11	13	14.0	20	3.67
12	11	11.0	15	2.75

# Technical specifications of the solar equipment

## • Ibersolar2122 Flat Plate Collector:

- Fluid capacity: 55 L/collector m<sup>2</sup>.
- Useful area: 2.16 m<sup>2</sup>.
- Efficiency:  $\eta = 0.72$ .
- U: 4.5 W/(m<sup>2</sup> · K).
- Position. Latitude:  $\Phi = 39^{\circ}48$  N.
- Orientation: South direction  $Z_s = 0^{\circ}$ . Inclination  $\beta = 45^{\circ}$  (used the whole year).
- N° of collectors: 25.
- $T_{out}$ : 60°C.

# Energy demand: 40 homes (20 of 2 bedrooms and 20 of 3 bedrooms)

• **Código Técnico de Edificación. Documento “Ahorro energía” (CTE-HE4. 4.1):**

– Total people:  $3 \cdot 20 + 4 \cdot 20 = 140$ .

Tabla 4.2. Valores mínimos de ocupación de cálculo en uso residencial privado

Número de dormitorios	1	2	3	4	5	6	≥6
Número de Personas	1,5	3	4	5	6	6	7

– Average of daily consumption:  
 $140 \cdot 28 \cdot 0.85 = 3332 \text{ L/day}$ .

Tabla 4.1. Demanda de referencia a 60 °C<sup>(1)</sup>

Criterio de demanda	Litros/día-unidad	unidad
Vivienda	28	Por persona
Hospitales y clínicas	55	Por persona
Ambulatorio y centro de salud	41	Por persona
Hotel *****	69	Por persona
Hotel ****	55	Por persona
Hotel ***	41	Por persona

– Solar minimum contribution: **50%**.

Tabla 4.3. Valor del factor de centralización

Nº viviendas	N≤3	4≤N≤10	11≤N≤20	21≤N≤50	51≤N≤75	76≤N≤100	N≥101
Factor de centralización	1	0,95	0,90	0,85	0,80	0,75	0,70

Tabla 2.1. Contribución solar mínima anual para ACS en %.

Demanda total de ACS del edificio (l/d)	Zona climática				
	I	II	III	IV	V
50 – 5.000	30	30	40	50	60
5.000 – 10.000	30	40	50	60	70
>10.000	30	50	60	70	70

### Energy demand calculation

$$\dot{Q}_{needed} = c_p * \dot{m} * (T_{out} - T_{in})$$

$$Q_{needed} = \dot{Q}_{needed} * n^{\circ} \text{ days}$$

$$c_p = 1 \text{ kcal/kg.K}$$

$$\dot{m} = 3332 \text{ L/day}$$

$$T_{out} = 60 \text{ }^{\circ}\text{C}$$

$$1 \text{ kcal} = 0.001162 \text{ kWh}$$

Month	N° days	Water T <sub>in</sub> (°C)	Energy demand Q <sub>needed</sub> (kWh)
1	31	10	6006.430
2	28	11	
3	31	12	
4	30	13	
5	31	15	
6	30	17	
7	31	19	
8	31	20	
9	30	18	
10	31	16	
11	30	13	
12	31	11	

### Energy demand calculation

$$\dot{Q}_{needed} = c_p * \dot{m} * (T_{out} - T_{in})$$

$$Q_{needed} = \dot{Q}_{needed} * n^{\circ} \text{ days}$$

$$c_p = 1 \text{ kcal/kg.K}$$

$$\dot{m} = 3332 \text{ kcal/dia}$$

$$T_{out} = 60 \text{ }^{\circ}\text{C}$$

$$1 \text{ kcal} = 0.001163 \text{ kWh}$$

Month	N° days	Water T <sub>in</sub> (°C)	Energy demand Q <sub>needed</sub> (kWh)
1	31	10	6006.430
2	28	11	5316.659
3	31	12	5766.173
4	30	13	5463.914
5	31	15	5405.787
6	30	17	4998.900
7	31	19	4925.272
8	31	20	4805.144
9	30	18	4882.646
10	31	16	5285.658
11	30	13	5463.914
12	31	11	5886.301

### Energy production calculation

$$Q_{produced} = G_g - Q_{conv} - Q_{rad}$$

$$G_g = \eta * \text{Incident solar radiation} * S_{abs} * n^{\circ} \text{ days}$$

$$Q_{conv} = U * (T_{absor} - T_{amb}) * S_{abs} * 60 * 60 * 24 * n^{\circ} \text{ days} * 2.78 \times 10^{-7}$$

$$Q_{rad} = \epsilon_{abs} * \sigma * (T_{absor}^4 - T_{amb}^4) * S_{abs} * 60 * 60 * 24 * n^{\circ} \text{ days} * 2.78 \times 10^{-7}$$

$$1 \text{ J} = 2.78 \times 10^{-7} \text{ kWh}$$

$$U = 4.5 \text{ W}/(\text{m}^2 \cdot \text{K})$$

$$\epsilon_{abs} = 1$$

$$\sigma = 5.67 \times 10^{-8}$$

$$\eta = 0.72$$

$$S_{abs} = 2.16 * 25 = 54$$

Month	N° days	Ambient T °C	Absorber T <sub>absor</sub> °C	Incident solar radiation kWh/(m <sup>2</sup> · day)	Energy demand Q <sub>needed</sub> (kWh)	G <sub>g</sub> kWh	Q <sub>conv</sub> kWh	Q <sub>rad</sub> kWh	Q <sub>prod</sub> kWh	% solar production
1	31	10.0	15	2.96	6006.430	3567.629	904.683	1061.155	1601.791	27
2	28	11.0	15	3.80	5316.659					
3	31	13.0	20	4.76	5766.173					
4	30	15.0	20	5.08	5463.914					
5	31	18.0	25	5.21	5405.787					
6	30	22.0	30	5.57	4998.900					
7	31	24.0	30	6.08	4925.272					
8	31	24.0	30	5.92	4805.144					
9	30	22.0	30	5.57	4882.646					
10	31	18.0	25	4.63	5285.658					
11	30	14.0	20	3.67	5463.914					
12	31	11.0	15	2.75	5886.301					



### Energy production calculation

$$Q_{produced} = G_g - Q_{conv} - Q_{rad}$$

$$G_g = \eta * \text{Incident solar radiation} * S_{abs} * n^{\circ} \text{ days}$$

$$Q_{conv} = U * (T_{absor} - T_{amb}) * S_{abs} * 60 * 60 * 24 * n^{\circ} \text{ days} * 2.78 \times 10^{-7}$$

$$Q_{rad} = \epsilon_{abs} * \sigma * (T_{absor}^4 - T_{amb}^4) * S_{abs} * 60 * 60 * 24 * n^{\circ} \text{ days} * 2.78 \times 10^{-7}$$

$$1 \text{ J} = 2.78 \times 10^{-7} \text{ kWh}$$

$$U = 4.5 \text{ W}/(\text{m}^2 \cdot \text{K})$$

$$\epsilon_{abs} = 1$$

$$\sigma = 5.67 \times 10^{-8}$$

$$\eta = 0.72$$

$$S_{abs} = 2.16 * 25 = 54$$

Month	N° days	Ambient T °C	Absorber T <sub>absor</sub> °C	Incident solar radiation kWh/(m² · day)	Energy demand Q <sub>needed</sub> (kWh)	G <sub>g</sub> kWh	Q <sub>conv</sub> kWh	Q <sub>rad</sub> kWh	Q <sub>prod</sub> kWh	% solar production
1	31	10.0	15	2.96	6006.430	3567.629	904.683	1061.155	1601.791	27
2	28	11.0	15	3.80	5316.659	4136.832	653.707	770.784	2712.341	51
3	31	13.0	20	4.76	5766.173	5737.133	1266.556	1549.046	2921.531	51
4	30	15.0	20	5.08	5463.914	5925.312	875.500	1081.825	3967.987	73
5	31	18.0	25	5.21	5405.787	6279.509	1266.556	1630.693	3382.259	63
6	30	22.0	30	5.57	4998.900	6496.848	1400.800	1887.547	3208.501	64
7	31	24.0	30	6.08	4925.272	7328.102	1085.620	1477.459	4765.023	97
8	31	24.0	30	5.92	4805.144	7135.258	1085.620	1477.459	4572.179	95
9	30	22.0	30	5.57	4882.646	6496.848	1400.800	1887.547	3208.501	66
10	31	18.0	25	4.63	5285.658	5580.446	1266.556	1630.693	2683.197	51
11	30	14.0	20	3.67	5463.914	4280.688	1050.600	1291.541	1938.547	35
12	31	11.0	15	2.75	5886.301	3314.520	723.747	853.368	1737.405	30

## Heat storage system calculation

Código Técnico de Edificación  
Documento “Ahorro energía” (CTE-HE4. 2.2.5)



$$50 < \frac{V}{A} < 180$$

V in L

A in m<sup>2</sup>

$$A = 54 \text{ m}^2$$

$$V_{\min} = 54 \cdot 50 = 2700 \text{ L.}$$

$$V_{\max} = 54 \cdot 180 = 9720 \text{ L.}$$

We choose a **3000 L** heat storage system.